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Technical Report No. 7

HIGH PRESSURE X-RAY STUDIES OF POLYMERS. II.

VARIATION OF PRESSURE WITH

TEMPERATURE IN THE DIAMOND-ANVIL CELL

by

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Prepared for Publication in the Journal of Polymer Science

October 15, 1976

Research Sponsored by the Office of Naval Research

Contract NOOO14-75-C-0540
Task Number NR 356-564

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SECURITY CLASSIFICATION OF THIS PAGE (When Date Entered) READ INSTRUCTIONS
BEFORE COMPLETING FORM REPORT DOCUMENTATION PAGE REPORT NUMBER 2. GOVT ACCESSION NO. CIPIENT'S CATALOG NUMBER Technical Report No. 7 TIPLE (MIN SUBILITY) HIGH PRESSURE X-RAY STUDIES OF POLYMERS III. YARIATION OF PRESSURE WITH Technical Repet TEMPERATURE IN THE DIAMOND-ANVIL CELL, BACT OR GRANT NUMBER(*) B. A. Newman, K. D. NØØØ14-75-C-Ø540 PERFORMING ORGANIZATION NAME AND ADDRESS 10. PROGRAM ELEMENT, PROJECT, AREA & WORK UNIT NUMBERS High Pressure Research Laboratory Rutgers University, College of Eng'g New Brunswick, N.J. 08903 NR 356-564 11. CONTROLLING OFFICE NAME AND ADDRESS 12. REPORT DATE Office of Naval Research (Code 472) October 15, 1976 Arlington, Virginia 22217 13. NUMBER OF PAGES 15. SECURITY CLASS. (of this report) Iling Office) Unclassified 154. DECLASSIFICATION/DOWNGRADING 6. DISTRIBUTION STATEMENT (of this Report Approved for public release; distribution unlimited. Reproduction in whole or in part is permitted for any purpose of the United States Government. TEMENT (of the abstract entered in Block 20, if different from Report) 8. SUPPLEMENTARY NOTES 19. KEY WORDS (Continue on reverse side if necessary and identify by block number) High Pressure, X-ray, Pressure Calibration, Diamond-Anvil Cell, Structure of Polyethylene at High Pressures. 0. VASSTRACT (Continue on reverse side if necessary and identify by block number) The pressure in the diamond cell X-ray camera was measured as a function of temperature. Contrary to the assumption of previous workers this pressure was not found to be constant with increased temperatures, the different thermal expressions of sample, pressure medium, diamonds and retaining ring combining to produce pressure increases of 100% over a 100% temperature range. (over) EDITION OF ! NOV 68 IS OBSOLETE E/H 0102-014-6601 | SECURITY CLASSIFICATION OF THIS PAGE (When Date & 09913

20. Continued:

In view of the fact that the diamond cell is frequently used to study the crystallization of polymers at high pressure, it should be noted that changes in pressure are equivalent to changes in the degree of supercooling. Since the crystallization kinetics and resulting polymer morphology are affected critically by even small changes in the degree of supercooling, conclusions drawn from investigations where the pressure was not directly measured should be regarded with caution.

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INTRODUCTION

High pressure X-ray diffraction and optical studies of polymers using the gasketed diamond-anvil cell have been reported by a number of investigators (1-5). The use of such a device is particularly interesting since crystal phase transitions and crystallization of polymers at high pressures and temperatures can be observed directly (5) or by X-ray diffraction (4). There are, however, several difficult experimental problems that must be overcome if a successful experiment is to be carried out. The first is to ensure that hydrostatic pressure is achieved in the device so as to avoid gross anisotropic distortion of the polymer sample. This can be accomplished if the sample in the gasket is surrounded by a pressure-transmitting fluid. The second is that an accurate method of pressure measurement must be developed for at least the range of pressures used in the study (6). Furthermore, there are other problems associated with the use of the device if high temperatures are introduced in addition to high pressures.

In this paper, the problems associated with the use of the diamond-anvil cell with combinations of high pressure and temperature are discussed. It appears in the literature that the pressure in the cell is assumed to be constant during temperature change and during crystallization. It is convenient to make this assumption and then compare thermal treatments in the diamond cell with high pressure differential thermal analyses (DTA) or dilatometric data. Both Bassett et al. (4) and Jackson et al. (5) made

comparisons with crystallization experiments carried out under constant pressure in DTA, although the former did discuss the problem that the pressure was not constant during crystallization. If the pressure in the diamond cell changes during the course of crystallization, then, of course, so does the degree of supercooling, and it is well known that this latter parameter is a critical factor in crystallization. Furthermore, an accurate measurement of pressure in the diamond cell at elevated temperatures is another associated problem. Optical methods based on ruby fluorescence cannot be used for precision measurements at temperatures above 200°C (7). The method utilizing the equation of state for NaCl developed by Dekker is not sufficiently accurate over the pressure range of interest for polymer studies (8). A method used by other workers is to measure the melting point of the pressurized polymer and compare this value to values obtained in a dilatometric device. This method certainly provides a measurement of pressure at the temperature where melting of the polymer is observed. If pressure constancy with temperature is assumed, then this method can serve a useful purpose. However, as already discussed, this assumption remains to be tested.

An alternative method of measurement of pressure at elevated temperatures has been developed by the authors, deriving the equation of state for hexamethylene tetramine (HMT)(9). A functional form for the equation of state was derived by consideration of the potential energies between non-bonded atoms in neighboring molecules, with due consideration for thermal vibrations. The parameters of

this functional form were determined by comparing the functional dependence with experimental data. With this more accurate technique available to determine pressure at various temperatures, it is possible to test the assumption of constancy of pressure in the diamond-anvil cell with varying temperatures.

The evidence that the pressure in the diamond-anvil cell can vary by as much as 100% over a 150°C temperature interval is presented here. It will be demonstrated that the pressure in the device is a non-linear function of temperature and that the pressure also depends on the relative volume of the components in the device, the sample material, the pressure standard, and the pressure transmitting fluid.

EXPERIMENTAL PROCEDURE

The experimental techniques employed in this study have been described elsewhere (3,6). A brass gasket 3/8 in. in diameter and 1/32 in. thick with an axial cavity 1/32 in in diameter was used. The gasket was inserted inside a resistance heater, and an iron-constantan thermocouple, together with a current-adjusting silicon rectifier controller, was used to measure temperature within ±0.1° accuracy.

Earlier workers (2,4) appeared not to have used a pressuretransmitting fluid, although our experiments indicated that, under these conditions, pressure gradients caused severe distortion of the sample. All our experiments were carried out using silicon oil as a pressure-transmitting fluid. It is believed, however, that the conclusions arrived at in this study apply equally to the case when no pressure medium is used. A small sample consisting of linear polyethylene (Marlex 6009) mixed intimately with powdered HMT was molded and deposited in the cavity and silicon oil added. Changes in the d-spacing of the (110) reflection of HMT were measured and, by using the equation of state for HMT (9), the pressure in the cavity determined. The sample was pressurized to some initial value and then the temperature raised in steps. After every temperature increment, the pressure was determined.

RESULTS AND DISCUSSION

Two separate experiments were carried out with two different samples and two different initial pressures. The initial pressure exerted on sample A was 4.1 kb and the initial pressure on sample B was 2.8 kb. The measured pressure on each sample at various temperatures is shown in Table 1. As the temperature increased, the pressure increased in a non-linear fashion as shown in Fig. 1. That this phenomenon was reversible was also observed by slow cooling of the sample and measurement of the pressure, unless the sample was melted, when crystallization on cooling led to an abrupt loss of some pressure (1-2 kbs).

A simple analysis to a first approximation of this situation throws some light on the pertinent features of this phenomenon.

(a) Case when no pressure medium is used. This is important, since some reports have been published of data obtained without use of a pressure medium. If the volume of a solid at zero pressure and the absolute zero of temperature is V_O, then according to Slater (9), the volume at some pressure P and temperature T can be assumed to be

$$V = V_0[1 + a_0(T) - a_1(T)p + a_2(T)p^2....]$$

where a_0 , a_1 , a_2 etc. are functions of temperature. In the case when no pressure medium is used and the solid is pressurized to some initial pressure P_i at room temperature T_r , some initial volume V_i can be expressed as

$$V_i = V_0[1 + a_0(T_i) - a_1(T_i)p_i + a_2(T_i)p_i^2 +]$$

The temperature of the sample is then raised to a value $T_i + \Delta T$, and we assume this causes the pressure to change by an amount Δp . If the thermal expansion of the solid α and the compressibility of the solid χ is approximately constant over Δp and ΔT , neglecting second-order and higher terms, we have the volume

$$V = V_i + \alpha \Delta T - \chi \Delta p$$

We will assume that the volume of the pressurized sample remains constant during the temperature increase. Actually, there may be some small change, but frictional forces exerted by the diamond facets, and the relatively low thermal expansion of the gasket material will ensure that V_i is approximately equal to V, in which case we have

$$\alpha \Delta T = \chi \Delta p$$

or
$$\Delta p = \frac{\alpha}{\lambda} \Delta T$$

This would imply a linear increase of pressure with temperature. Moreover, if changes in the α and the χ with temperature and

and pressure are taken into consideration in the above analysis, the pressure increase will be nonlinear and even more exagerated at higher temperatures. Another factor not accounted for in the analysis is the change in specific volume that occurs during melting and recrystallization.

(b) Case when a pressure medium is used. This is the case actually investigated in some detail. If V_p , V_h , and V_m are the volumes of the polymer sample, the pressure standard HMT, and the pressure medium respectively, a similar analysis will lead to

$$(\alpha_{\mathbf{p}} \mathbf{V}_{\mathbf{p}} + \alpha_{\mathbf{h}} \mathbf{V}_{\mathbf{h}} + \alpha_{\mathbf{m}} \mathbf{V}_{\mathbf{m}}) \Delta \mathbf{T} = (\chi_{\mathbf{p}} \mathbf{V}_{\mathbf{p}} + \chi_{\mathbf{h}} \mathbf{V}_{\mathbf{h}} + \chi_{\mathbf{m}} \mathbf{V}_{\mathbf{m}}) \Delta \mathbf{p}$$
or
$$\Delta \mathbf{p} = (\frac{\alpha_{\mathbf{p}} \mathbf{V}_{\mathbf{p}} + \alpha_{\mathbf{h}} \mathbf{V}_{\mathbf{h}} + \alpha_{\mathbf{m}} \mathbf{V}_{\mathbf{m}}}{\chi_{\mathbf{p}} \mathbf{V}_{\mathbf{p}} + \chi_{\mathbf{h}} \mathbf{V}_{\mathbf{h}} + \chi_{\mathbf{m}} \mathbf{V}_{\mathbf{m}}}) \Delta \mathbf{T}$$

where α_p , α_h , α_m are the respective thermal expansion coefficient and χ_p , χ_h , χ_m the respective compressibility of the sample, HMT, and the medium.

A simplification of the above equation can be achieved by neglecting V_h since it is small compared with V_p and V_m , and by assuming $V_p = V_m$, that is, very close to the actual situation, then

$$\Delta p = (\frac{\alpha_p + \alpha_m}{\chi_p + \chi_m}) \Delta T$$

This does predict the dependence of pressure on temperature in the diamond-anvil cell: linear dependence if α_p , α_m , χ_p , and χ_m are assumed to be constants and non-linear dependence if α_p , α_m , χ_p and χ_m are functions of pressure and temperature.

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TABLE I.

ole A	Pressure				
TEMPERATURE (°C)	kg/cm²	kb			
24	4.01	4.09			
100	4.58	4.67			
150	5.42	5.53			
180	5.87	5.99			
190	6.13	6.25			
200	6.28	6.40			
210	6.57	6.70			
220	6.72	6.85			
240	7.76	7.91			
260	8.68	8.85			
280	10.04	10.24			
290	10.42	10.63			
ple B	Pressure				
TEMPERATURE (°C)	kg/cm²	kb			
24	2.72	2.77			
150	4.26	4.34			
180	4.47	4.56			
200	5.37	5.48			
200		6.15			
215	6.03	6.15			
	6.03 6.70	6.15 6.83			

5.

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Fig. 1. Variation of Pressure with Temperature in High Pressure Diamond-Anvil Cell.

